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Beetle MOLDING MATERIALS

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Betle MOLDING MATERIALS

(1146)

AMERICAN CYANAMID COMPANY
BEETLE PRODUCTS DIVISION
30 ROCKEFELLER PLAZA
NEW YORK, N.Y.

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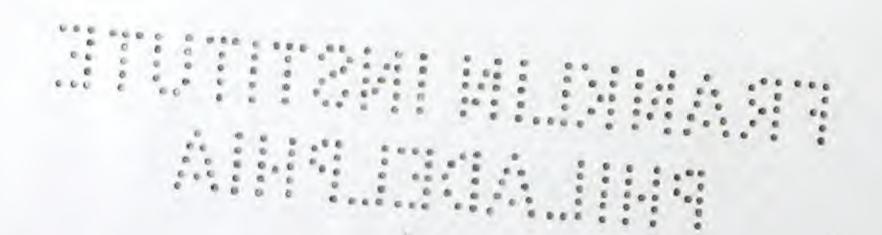




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INTRODUCTION

This booklet, entitled "Beetle," is issued by the Beetle Products Division of the American Cyanamid Company to bring up to date pertinent information regarding ureaformaldehyde molding compounds sold under its trade name. It is of importance to note, at the outset, that the plastics industry is not static and that data contained here will be subject to continued modification as the result of improved molding technique and improved materials.

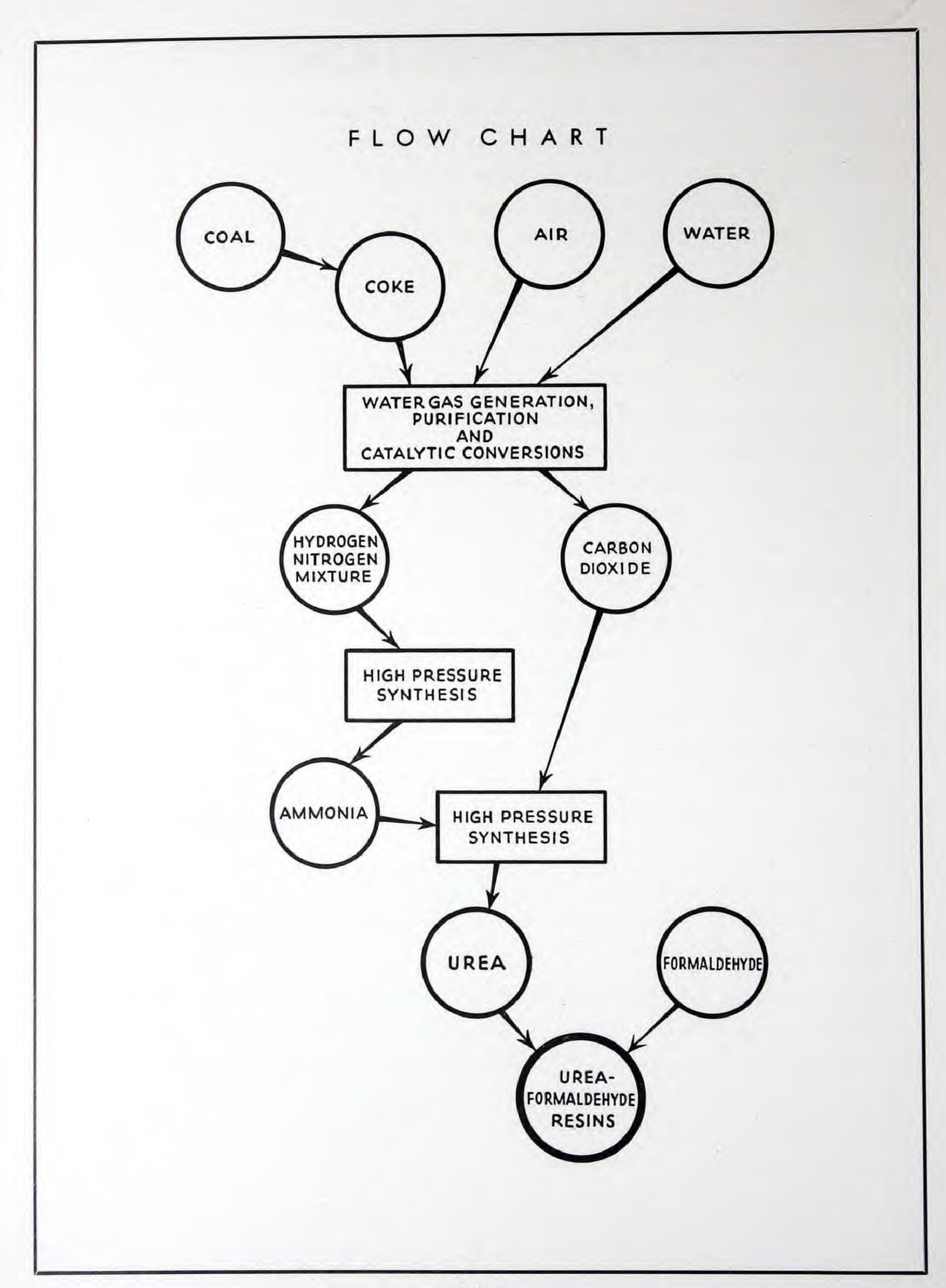
Although our discussion will be chiefly confined to the use of urea-formaldehyde resin in the form of a molding compound, it will be of value to the reader to mention that this basic resin, because of its intrinsic properties, finds many applications in other forms.

The uncured urea-formaldehyde resin is a colorless solution, fusible and partially soluble. When subjected to high temperatures, this resin undergoes a rapid chemical change and becomes insoluble, infusible, odorless, tasteless—in general, chemically inert. It is, therefore, a thermo-setting or heat-hardening resin. In the form of a solution, this resin is used for the construction of translucent or opaque laminated sheets; for the manufacture of cold-setting cements; in baking enamels; as plywood bonds and many other applications.

In combination with a finely divided alpha cellulose filler, the resin is sold as a molding compound, either in the form of a granule or a powder. Since the basic resin is colorless and the cellulose filler is a pale white, the molding compound in its natural unpigmented state will give pearl white translucent moldings. Through the addition of dyes or pigments in the manufacture of the molding compound, practically any color, either translucent or opaque, may be produced. Since the color of Beetle is due to these added coloring agents, the material is extremely color fast and as color stable as are the best dyes or pigments available.

Beetle molding compounds are molded in steel dies under the combined action of heat and pressure. The process is much the same as that used for the molding of other thermo-setting compounds.

In this book we shall give the route of our molding compound from the plant to the molder, and eventually to the consumer. We shall outline the best current molding practice, properties of finished parts and pertinent information regarding piece design and application. Naturally many problems may arise which require discussion with our technical representatives or laboratory technicians: such service is readily available to those requesting it.



BEETLE MOLDING MATERIALS

Beetle molding compounds are supplied in the forms of powder or granules, differing from each other in relative density or bulk.

Beetle Powder has a compression ratio of about 3.7 and therefore requires larger mold loading space than does the more dense material. Beetle powder produces parts having an excellent finish and parts which are slightly stronger, particularly around heavy inserts. However, because of the powder's fluffiness and bulk, difficulties may be experienced in handling and measuring mold charges; its use is generally confined to those plants having specialized equipment to handle it.

Beetle Granular, the standard form of the compound, has a compression ratio of 2.5. Although the granular form is somewhat more expensive, it affords offsetting economies in the handling, loading, and measuring operations. Granular Beetle may be tabletted, thereby further facilitating the weighing and loading of mold charges. Experienced molders are of the opinion that granular Beetle affords many economies in that it presents a form of material more easily handled in the plant.

Since Beetle compounds may be obtained in practically any translucent or opaque color, and since they are purchased because of their beauty as a finished part, Beetle is produced in "hospital clean" conditions.

This material, after being produced in an air-conditioned plant, is packed in composition drums with "Leverpak" closure. Normal container size is 200 lbs. content and measures without cover 22" diameter by $26\frac{1}{2}$ " tall, or $20\frac{1}{2}$ " in diameter by $30\frac{1}{2}$ " tall. Small size drums have telescoping composition tops and are available on request and on payment of a slight additional fee.

In both powder or granular forms, Beetle is supplied in many plasticities designed to meet job specifications and molding conditions. It may be safely said that throughout the molding industry, no two molds are exactly alike, nor do any two molds present the same conditions of pressure, restrictions to flow, or other variables. To meet these conditions, Beetle manufactures a wide range of materials with regard to plasticity:

- 1. Very Soft—Material designed to meet severely under-pressured molding conditions. Same rapid cure as for the hard flows.
 - 2. Soft-Material designed to operate in molds slightly under-pressured.
- 3. Medium Soft and Medium Hard—This is customarily used as a general purpose material. It possesses a uniform flow, excellent surface appearance, rapid cure, and is very gas free. Moldings have been consistently produced in this material from small buttons to large housings.

- 4. Hard—This material is used to mold small parts such as buttons and closures, and because of its hardness it produces an unusually excellent finish.
- 5. Very Hard-This material is similar to the hard type and has been developed for over-pressured molds. Used principally for buttons.

It is important to note that the above variations are produced without sacrifice of quality or rate of cure. Soft materials require no more curing time than the harder varieties. When compared at the same temperature, the cure rates of all types are practically the same.

In addition to these standard types we also manufacture several special grades to fit particular conditions of exposure.

PROCESSING OR MOLDING BEETLE

On receipt of Beetle materials at the shop, unless they are immediately used, they should be stored in a cool, dry place. Dirt and moisture are the enemies of clean, light-colored urea molding compounds. They should be protected by adequate covering and sealing, just as carefully as the highly polished dies are protected from dirt and moisture.

Dirt means rejects; excess moisture means poor appearance and detracts from the correct flow of the product. Damp material also causes sticking to preform punches.

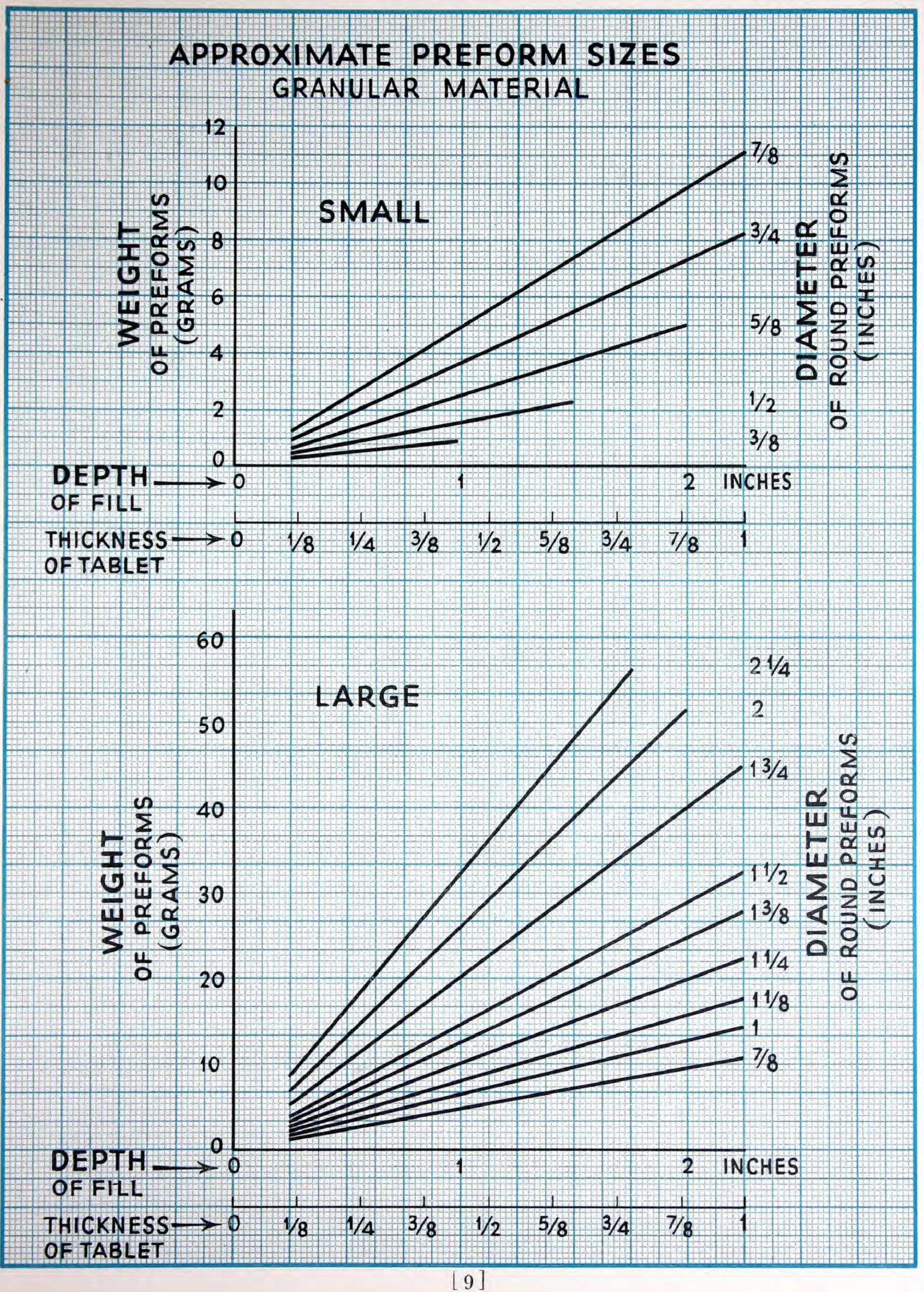
Cold storage and cold weather protect the urea compound against alteration of its flow characteristics, but for best working conditions the compound should be reasonably warm before being charged into the die. Drums of material in winter take from 24 to 48 hours to become thoroughly warmed. The time will depend on weather and storage conditions. If the material is cold it should be placed in a room where temperatures run from 80° to 100° F. for the above period. The use of hot pipes or extreme temperatures should be avoided.

Excessive moisture can best be avoided by tightly closing the drums, or by rolling them prior to use, if the outer layers have become damp.

When applications which require absolute cleanliness are to be molded, such as lighting reflectors, it would be wise to consult with a technical representative of Beetle regarding methods of handling the compound from drum to die.

PREFORMING OF UREA MOLDING MATERIALS

With all quantity production of small parts in multi-cavity dies, it is most convenient and economical to charge the mold with tablets by means of a loading board. In this way the material is automatically weighed and densified, and the minimum quantity necessary to make each piece is rapidly placed in all cavities in one motion.



Beetle may be preformed in any of the standard machines that are used with phenolic compounds. There are two types, the single punch machine and the rotary. The rotary is most suitable for quantity production of round preforms up to one inch in diameter. The larger single punch machines are best suited for pills one inch in diameter to two and one-quarter inches. Although multiple punches are supplied for the large single stroke machine, it is generally found that the uniformity of tablet weight is not so good as that obtained with the smaller single punch machines or with the rotary.

Points to be noted with regard to preforming Beetle:

- 1. Ureas demand higher pressures than phenolics to produce similar sized pills. On a single stroke machine this will mean a smaller maximum size. For example, a certain type single stroke machine is rated to produce a three-inch diameter maximum size phenolic pill. The upper limit for ureas on this machine is between 2½" and 2½". In general, rotary machines are able to handle phenolics and ureas interchangeably, so that only in the extreme sizes is it necessary to consider the excess pressure needed.
- 2. Since many molders make their own dies and punches, a few words should be said about their design. The most important matter here is the clearance between punches and dies. There is air between the granules and it must be permitted to escape through these clearances when the compound is compressed.

	BETWEEN THE PUNCH AND THE	DIE
Nominal Size	Clearance—Upper Punch	Clearance—Lower Punch
1/4" diameter	0.003	0.002
1/2" "	0.003	0.003
3/4"	0.005	0.004
1,,,	0.007	0.005
11/2" "	0.010	0.007
2"	0.012	0.010
21/2" "	0.014	0.012

Larger clearances between punch and die cause dusting or splash of the material from the dies, and a fin will be formed at the pill edges.

Dies should be checked occasionally for wear. After considerable use their bores may become barrel shaped, causing expensive pill breakage on ejection from the die.



Handles and knobs of molded Beetle are smooth, pleasing to the touch, and colorful. Qualities of chemical inertness, moisture resistance, strength, high insulating value, and ready adaptability to design requirements, make Beetle the ideal material for handles and knobs in matching or contrasting colors.

The die should be hand polished axially to remove circular grinding streaks which impede tablet ejection. It is well to produce a slight flare outward—about .002" increase in diameter per inch of depth—to permit easy pill ejection.

- 3. Among the operating details, temperature is an important factor. Since urea compounds will not produce good solid preforms at low temperatures, it is wise to allow the material to come to room temperature before preforming it.
- 4. Tablet machine operators often add stearate of zinc to the material to facilitate ejection of the pill. Difficulties with ejection are usually due to cold equipment, new, unlubricated die surfaces, recently cleaned dies, improperly polished parts, or damaged and scratched equipment. Whatever the reason, stearate should be used sparingly, and with constant examination of molded pieces, since there is danger of producing parts with poor surface finish or white stearate splotches. We believe it advisable, whenever possible, to adhere to the practice of dry cleaning dies rather than use of solvents.

Before preforming a drum of material, roll the drum sufficiently to obtain a uniform mixture of the particles. More uniform pill weights will result. Full drums are more difficult to mix than those having 15% to 20% of their contents removed.

PREWARMING Urea-formaldehyde material is most readily molded when warm. Because of its resistance to heat transfer, it is sometimes difficult during the short molding cycle to warm a large mass of material uniformly, and to obtain the same degree of softness or moldability throughout the charge. The closer the material can be brought to its molding temperature before being charged into the die, the better will be the piece.

On otherwise difficult jobs, prewarming will produce a piece that has not only a superior appearance but which will also be more resistant in service conditions. Since the material when hot reacts quickly and becomes unmoldable, prewarming must be carried out with close control of temperature and time of heating. Material charged into the mold at 180° F. to 190° F. gives the best results. To heat the material quickly to this temperature, it must be spread out in thin layers on a heated surface, or agitated in a heated rotating container to expose all portions for a uniform time to a heated surface. Heating surfaces should not exceed 250° F. and there should be enough surface so that not over 8 to 10 minutes is required to heat the material.

Prewarming is at best a critical operation and not recommended except in cases of difficult molding or when extra quality is required in a finished piece.

FLOW As a general rule, urea-formaldehyde materials have an optimum flow rate at which they should travel in the die, and move to fill out the piece being made. Too rapid a flow caused by too much mold pressure will not permit sufficient heat and pressure to be



Ivory is one of the most popular of Beetle colors. Because it harmonizes with virtually any color scheme it is widely used for products and appliances that find their way into the home.

transferred from mold to material, so that non-plastic portions of the charge are forced into place, leaving blisters, opaque spots, or undensified areas. Too slow a flow will permit overheating and prehardening of the charge, thus preventing complete closing of the mold.

The range of flows available in Beetle material is such that the softest types can be molded at approximately half the pressure required for the hardest types.

Because of certain conventional relations between the pressure capacity of a press and the area of a mold which can be mounted therein, two statements may be made.

- 1. Large, deep draw moldings which require high unit molding pressures tend to be under-pressured. Soft materials are therefore required.
- 2. Small, flat pieces requiring less unit pressure and having less total molded area for a given mold size tend to be over-pressured. Stiff materials are therefore required.

Between these extremes lies a wide range of conditions. There is a wide range of flow characteristics available in Beetle materials to meet these conditions without sacrifice of quality or cure time.

MOLDS Pure urea resins, unlike pure phenolic resins, do not fuse to a semi-liquid state through the application of heat alone. Urea molding compounds require both heat and pressure to cause them to flow and fill all parts of the mold; dies must therefore be designed to insure the even application of pressure and heat over the entire area of the part.

Beetle may be molded in either a flash or semi-positive type mold, depending on the shape of the piece required and the quality of product desired.

The flash type mold is best suited to produce small pieces of little or no draw, such as buttons or closures. To secure the necessary density in pieces formed in such a die, it is suggested that pills or preforms be used. Sometimes with pieces having complicated shapes or variations in sections it is necessary to make the mold slightly semi-positive.

The flash mold is not suited to produce pieces having a heavy cross section, such as knobs and gear shift balls, or parts requiring a long draw, such as tumblers.

The semi-positive mold is best suited to fabricate ureas, because it applies an even, positive pressure on the compound throughout its flow. Parts having a long flow or draw, such as tumblers, radio cabinets, or clock cases, or parts having a thick cross section, should be molded in such dies.

The use of a semi-positive die will result in a saving of raw material, since the cavity is practically closed and will not permit much of the compound to escape as flash.

Molds should be designed so that all surfaces of the die are approximately the same distance from the source of heat. The added expense of coring the mold will be offset

to a great degree by the faster production of better and more uniform parts. Differentials in cure at various localities of a large piece resulting from poor heat distribution in the die can lead to a differential in shrinkage which in turn may lead to cracking.

In order to maintain the proper mold temperature it is vital to remove the condensed steam as rapidly as possible. This requires a well-made, reliable type of steam trap with strainer.

Sample molds are usually heated by conduction and are sometimes cheaply constructed. The frequent removal of this die from the press for unloading purposes results in a fluctuation of the mold temperature. Care should be exercised to bring the die back to correct molding temperatures, if the production of poor pieces is to be avoided. The calibre of pieces produced from such a mold is not necessarily indicative of what may be produced from a permanent steam channeled die.

THE MOLDING OF BEETLE

TEMPERATURE Beetle may be molded at temperatures as low as 275° F. and as high as 340° F. Below 275° F. parts appear to be blistered, except after an extremely long cure. Above 340° F. parts may burn and whiten. The entire process of carrying molding powder through its plastic state into a hard finished piece is accelerated by the higher mold temperatures.

Ordinarily the highest mold temperatures which permit the material to remain in its plastic state long enough for complete closing, and breathing if necessary, are the most economical to use. Lower temperatures produce parts with a better finish and tend to reduce flow marks.

Small parts, where the bulk of material to be heated is small and the flow short, are generally run at high temperatures.

Large parts, where the material flows a great distance and therefore more time is required for mold closing, are run at the lower end of the temperature range.

MOLDING PRESSURES Molding pressures required for ureas are usually higher than those required for phenolics, particularly for long draw pieces. Buttons, closures, and similar small parts made in flash molds, can be formed at 2,000 pounds per square inch of projected area. By the latter is meant the total area of the molds, including the flash lands. If a higher finish is required a more stiffly flowing Beetle must be specified and the molding pressure raised accordingly — possibly to 3,000 pounds per square inch of projected area.

Housings, tumblers, and such parts having a long draw, require higher pressures. A rule of thumb may be used by setting 3,000 pounds per square inch of projected area as the basic molding pressure, to which should be added 700-1,000 pounds per square inch for each additional inch of vertical draw. This rule applies when standard materials of standard plasticity are used.

Pieces of long draw having a thick cross section require less pressure than do draw pieces of thin cross section.

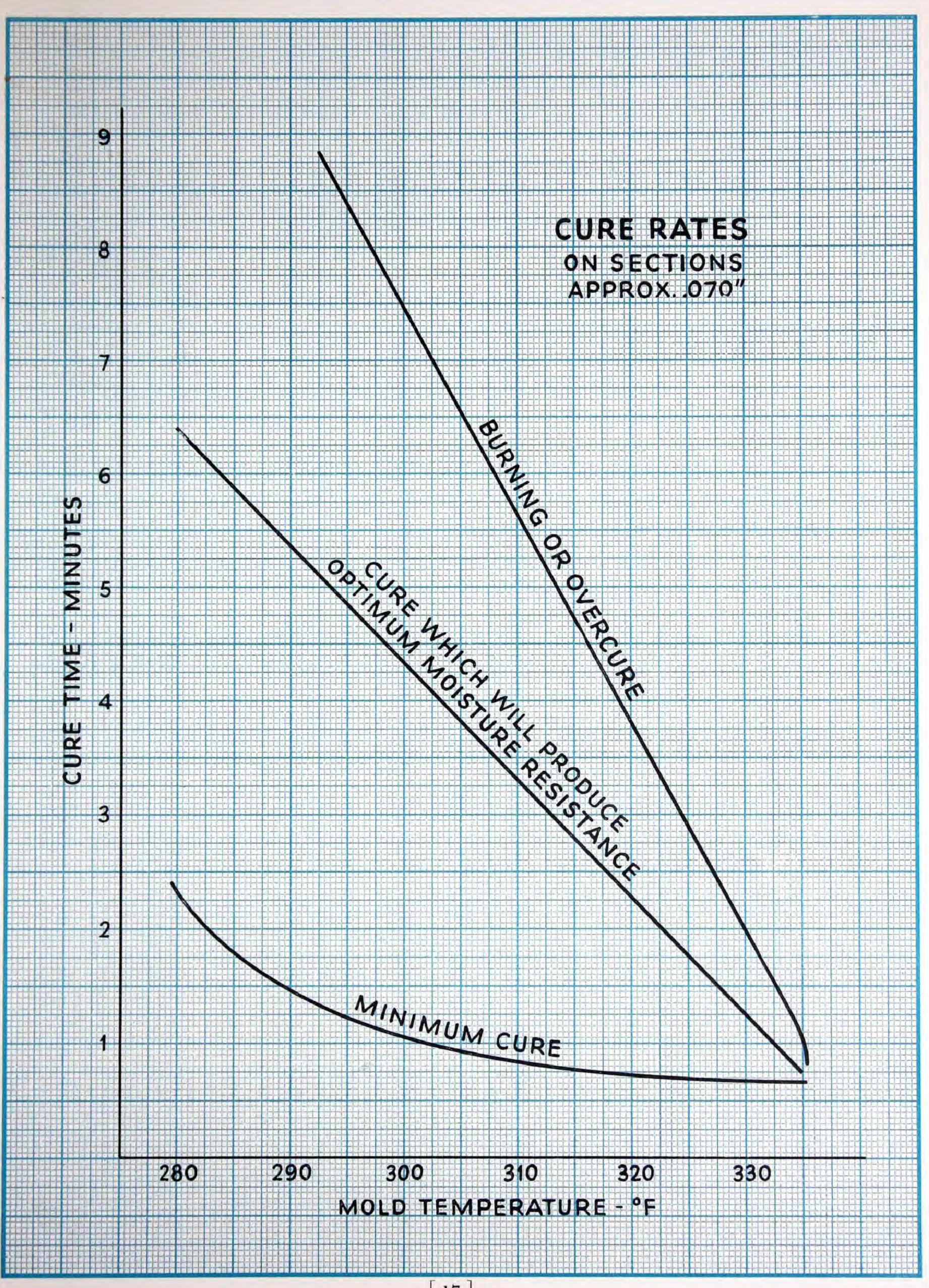
Table II below will summarize the above paragraphs.

CURE It is common knowledge that higher mold temperatures will permit shorter cures with resulting faster production rates. However, the highest permissible temperature is limited by the amount of flow required, and the general complexity of the molded piece. The relationship of heat and cure time in a given part may be seen by consulting the accompanying graph:

TABLE II-APPROXIMATE MOLDING CONDITIONS

Part	Area Projected Sq. Inches	Draw	Section Thickness Inches	Number of Parts per Pound of Material	Mold Tempera- ture Fahrenheit	Molding Pressure Tons per Cavity	Cure Time	Type of Mold
Buttons	1/4-2	_	3/32-5/32	150-1000	310–340	1/2-3	20 Secs. to 1 Min.	Flash
Closures	1/2-5	1/2-1	3/32-5/32	30–200	305–325	1-9	40 Secs. to 2 Min.	Flash or Semi-Positive
Wall Plates	15–25	_	3/32-1/8	12-20	310–320	20-35	50 Secs. to 2 Min.	Flash or Semi-Positive
Razor Housings	8-12	3/4-1	1/16-1/8	10-20	300–315	15-25	2-3 Min.	Semi-Positive
Housings Small	25–40	2–4	3/32-1/8	1-3	295–315	50-100	2-4 Min.	Semi-Positive
Housings Large	70–200	5-9	1/8-3/16	1-4 Lbs. per Piece	285–305	150-1000	21/2-5 Min.	Semi-Positive
Lighting Reflectors Large	200-400	3–10	5/64-7/64	1-4 Lbs. per Piece	280–300	600-1500	3–5 Min.	Semi-Positive

Buttons and closures can be molded at higher temperatures and at shorter cures because of the absence of flow and because the small mass of material may be quickly heated. Larger pieces requiring a greater flow and the uniform heating of greater masses of material require a longer cure at lower temperature.



The first effect of cure is to transform a soft, opaque and amorphous mass into a rigid, translucent molded part. Further cure improves some of the physical properties of the piece such as its resistance to moisture and its strength. Too long a cure burns or whitens the part and may, if too long continued, damage the die surface. On parts where shrinkage is a problem, prolonged cure is not advantageous as shrinkage of the part is increased.

The test for cure of a molded part should be based on the eventual use of the part.

Housings, lighting reflectors, as well as novelty items which require no special resistance to attack of moisture or solvents, are suitably cured when parts are blister- and gasfree when removed from the mold.

Tableware, closures, buttons, and parts coming in contact with liquids or solvents, should be cured long enough so that they show no attack or loss of gloss after one-half hour immersion in boiling water.

Parts having heavy sections, such as handles or knobs, should be sawed through the thickest section and inspected for uniformity of the molding. Short cures show a white core beneath the surface. This will cause cracking of the surface and should be eliminated by a longer cure or a change in the molding cycle.

Savings can often be made by adjusting the cure to the requirements of the part being molded.

It is possible as a production control test on a molded part to measure its percentage of water absorption after 15 to 30 minutes immersion in boiling water. Parts cured to the same degree will have the same percentage of absorption, and variations in cure can be detected in this way.

The simplest mold closing cycle which will produce good parts is always preferable. The primary objective to keep in mind in molding Beetle is that the mold charge should be heated throughout before the mold is closed. Good parts are often more easily produced by a short interruption of flow after molding pressure is first applied.

In the case of long draw pieces, the mold is closed very slowly. Depending upon the weight of the charge and shape of part, the closing operation may take from thirty seconds to one minute.

If small parts are to be produced in flash molds, the procedure is to close the mold to the point where the flash has ceased flowing, then breathe the die quickly, and close for final cure. In many cases the breathing operation may be eliminated.

If difficulty is experienced from trapped air or gas, the material may be preheated 10-20 seconds with the die nearly closed. The die is then momentarily opened, and allowed to close fully. Complicated cycles are hard to reproduce uniformly and can often be simplified. Change in mold temperatures or in flow characteristics of material aid in simplification of the cycle.



Beetle housings, such as this clock case, provide protection for the instrument and insure lasting beauty. Molded in one piece, they are ideal for assembly line production methods.

Urea-formaldehyde materials in a mold flow somewhat as would be expected of a lump of ice in a mold just warm enough to melt the ice. As the mold's heat softens the outer portions of the charge in contact with the metal, the softened compound flows under pressure and exposes relatively cold, unsoftened material to the mold's heat. This process continues until the die is closed. This compound remains soft for a very limited space of time, and under continued heat quickly hardens and resists further flow.

FINISHING OPERATIONS The flash or fin on small parts such as buttons or closures may be removed by tumbling these parts in a wooden barrel. If rough finishing is required, small wooden pegs or burnishing balls are mixed with the pieces and tumbling continues for about ten minutes.

Tumbling barrels are usually driven at about 20 to 40 R.P.M. If the parts are thin and easily chipped, the speed of rotation should be kept under 30 R.P.M.

Molded urea parts coming from the die bear the polish of the mold surface. If this is to be improved upon, small parts may be tumbled with a wax polish or waxed wooden pegs from one to two hours. If an unusually high polish is required a small amount of abrasive substance may be used, and the tumbling should continue for about six hours.

If the parts are large, with thin sections, or have heavy inserts which might become broken or clogged with the polishing compound, they should be finished on a sand belt or buffing wheel.

Filing is sometimes used to remove flash, but generally as a last resort. It is sometimes necessary in the spaces formed at louvres, dial openings, and knob holes on radio cabinets. Ureas are very hard, and filing, especially with a coarse toothed file, tends to start small cracks which may extend and open up as the piece ages.

On large parts, where possible, flash should be removed by a fine sanding wheel. Care should be taken to keep the plastic cool at the point of contact.

If a mold is well polished, Beetle parts made therein will have an excellent lustrous polish. No further finishing operations are necessary except the removal of flash or fin.

CORRECTION OF MOLDING DEFECTS

Undercure—In general undercure of a molded part results in blisters or opaque spots. An odor of formaldehyde is also noticeable. The symptoms of undercure—blisters and opaque spots—may also be due to improper mold closing, and if a longer cure does not remove them, the closing of the die may be slowed down, or the mold may be breathed to remove the fault.

Overcure—Overcure is indicated by a whitened surface on the part, and if sufficiently severe, is accompanied by a fishy odor. Overcure may be corrected by reducing the mold temperature and/or reducing the cure time.





No painting or polishing is necessary. The manufacturer of this scale reported his housing costs reduced 75 per cent when the Beetle model was adopted. Four molded parts provide the complete case for the delicate mechanism — simplifying the assembly job.

Flow Lines—Flow lines on a given part are frequently removed by a slower mold closing and lower mold temperatures. In extreme cases prewarming of the compound is necessary.

Low Density Areas—These areas may be due to insufficient mold charge, the result of too free flowing material, causing it to spurt out of the die, too rapid a mold close, or faulty die construction.

Water Resistance—In a given material water resistance is a function of cure. Both too long and too short a cure will produce poor water resistance. Generally the *best* results are obtained by fairly long cures at medium temperatures. Special varieties of Beetle are available where the optimum water resistance is desired. Actual immersion and weighing tests on the part in question are the best methods of determining the optimum cure for a given part.

Heavy Fins—Heavy fins on a molded part may be the result of several causes, and a remedy should be sought by checking the following factors:

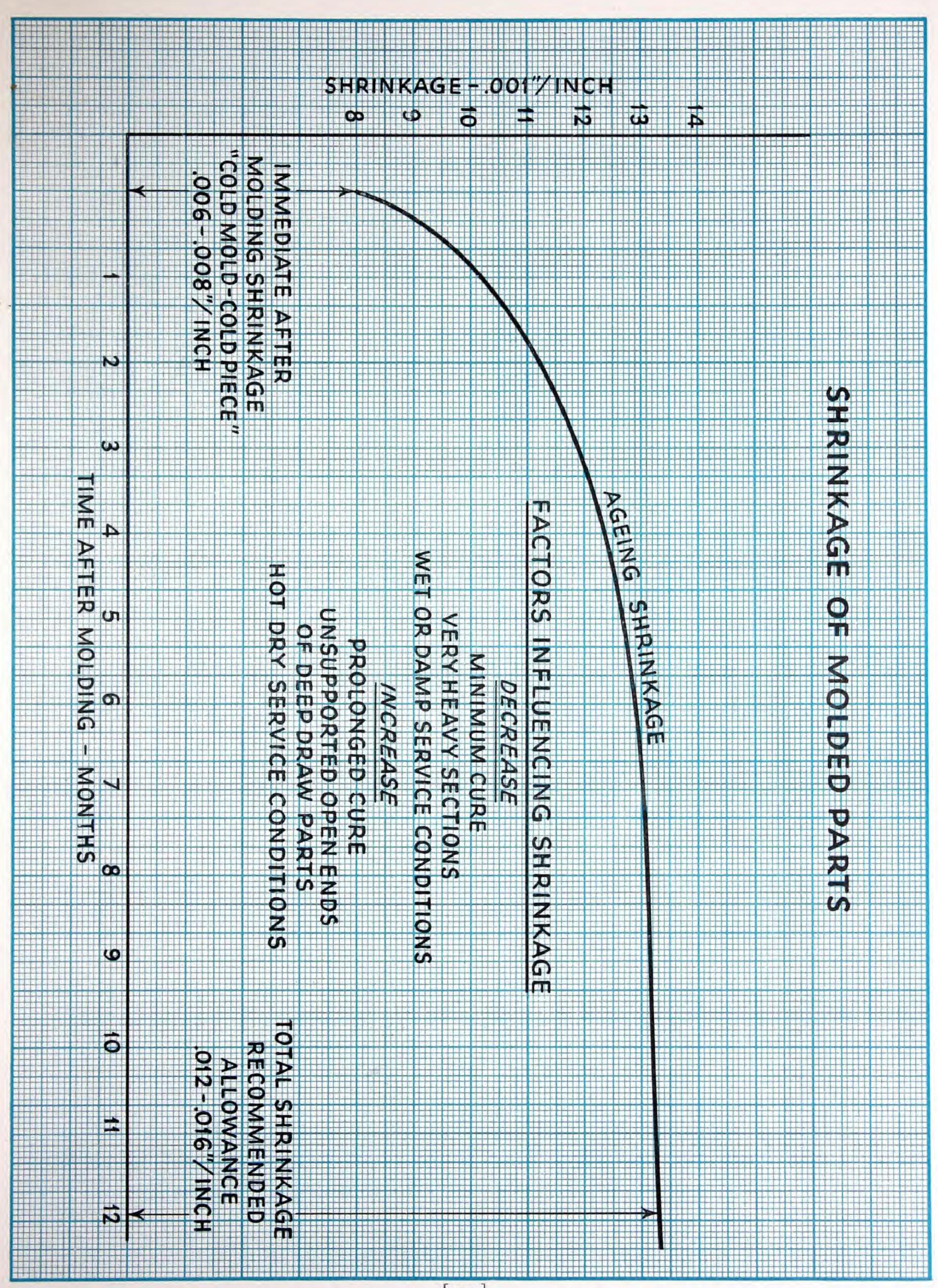
- 1. The mold should close evenly and be properly aligned.
- 2. Charges of material should not be too great.
- 3. Mold closing time should not be prolonged more than necessary.
- 4. Mold temperature should not be too high.
- 5. Material's flow characteristics should not be too stiff.
- 6. Semi-positive clearances should be ample.
- 7. New molds may be troublesome until "broken in."

Warping—Warping of parts is best counteracted by cooling the molded parts on a form or shrink block. Only a short time is necessary for this operation and successive parts can be placed on the forms while others are molding. A shrink block will not eliminate shrinkage—it will control it.

STORAGE OF FINISHED PARTS Molded ureas respond to warm, damp weather by swelling and to a dry atmosphere by shrinking. If a molding is at all critical with regard to size, if it is on the borderline of dimensional tolerances, it should not be stored in a hot, dry room. Moldings undergo the least dimensional change and strain if they are kept at about 65-70° F. and a relative humidity of 65%.

SHRINKAGE One of the most important factors to consider with regard to finished urea parts is the matter of dimensional change or shrinkage. In order to prevent assembly and service difficulties on molded parts where dimensional tolerances must be held, a correct allowance for shrinkage is essential.

There is an initial shrinkage of ureas which occurs immediately after a part is removed from the die. In addition, further aging shrinkage takes place over a prolonged



period of time, and is greater in hot, dry atmospheres than in moist, cool air. If the moisture in the air is sufficiently great, the piece may swell.

Initial shrinkage from cold mold size to cold finished molding runs .006-.008" per inch. After-shrinkage or aging shrinkage may run from half to once again this amount, so that where design permits, the full .012-.016" per inch should be allowed.

Summarized in the graph are the shrinkage data for Beetle molding materials.

PROPERTIES OF BEETLE MOLDING MATERIALS

GRANULAR

Size of Particle—16 mesh*

Apparent Density—.55-.60

Specific Volume—45-55 cubic inches to the pound Compression Ratio—2.5

Preform Possibilities—Excellent

POWDER

Size of Particle—200-300 mesh
Apparent Density—.4
Specific Volume—65-70 cubic inches to the pound
Compression Ratio—3.7
Preforming Possibilities—Poor

PROPERTIES OF FINISHED PARTS

Physical Properties —

Specific Gravity—

Weight per Cubic Inch-

Flexural Strength—

(ASTM D-48-34T)

5"x 1/2" x 1/2" bar, supports 4" apart, loaded in center

Flexural Strength, Dynstat

1.5 x 1.0 x 0.2 Cm.

Compressive Strength-

(ASTM D-48-33)

Tensile Strength-

(ASTM D-48-33)

Impact Strength, Dynstat

1.5 x 1.0 x 0.2 Cm.

Impact Strength, Charpy

Unnotched bar 5"x 1/2"x 1/2"

1.45-1.50

0.85-0.89 oz. (24-25 grams)

10,000-13,000 pounds per sq. in.

11,000-15,000 lbs. per sq. in.

20,000-24,000 lbs. per sq. in.

5,500- 7,000 lbs. per sq. in.

10-12 cm. kgs. per sq. cm.

1.2-1.4 ft. lbs.

^{*}A range of particle sizes is available to give an aggregate with optimum flow in feed hoppers, and also the best surface finish on the molded piece. Maximum particle size 16 mesh U. S. Std.



The smooth, wear-resistant surface of Beetle is ideal for products which must stand the abuse of constant handling in use. The color is in the material itself-there is no surface coating to chip or wear off.

Rockwell Hardness-

(ASTM D-229-34T)

1/4" ball-100 kg. load

78.9

Distortion Under Heat-

(ASTM D-48-39)

130° C .- 140° C.

Coefficient of Heat Expansion-

0.00001-0.00002 inch per inch per degree F. These values apply for temperatures from 100° F. and lower. At higher temperatures a slight shrinkage occurs which will reduce the apparent expansion. This must not be confused with mold shrinkage.

Burning Rate-

Very slow

Machining Properties—

Fair

Softening Point-

None

Water Absorption—

Piece .050" thick

Total immersion 24 hours at 25° C. I to 3% by weight

Weather Resistance—

Fair

Cold Flow-

None

Operating Temperature Maximum—

170° F.

Color-

Any color from a translucent white

Electrical Properties —

Dielectric Strength, Step-by-Step Method (ASTM D-149-36T)

Thickness of section 0.080"

25° C. room temperature 100° C. (212° F.) under oil 300-385 volts per mil.

100-140 volts per mil.

Volume Resistivity—Megohm—Cm.—(Electrical Testing Laboratory Report No. 138291)—

After 48 hours at 60% relative humidity

106-107

After 24 hours immersion in water

105-106

Surface Resistivity—Megohms—(Electrical Testing Laboratory Report No. 138291)—

After 48 hours at 60% relative humidity

3-10 x 106

After 48 hours immersion in water

0.02-0.11 x 106

Power Factor and Dielectric Constant—

Low Frequency—60 cycles—

Power Factor

Dielectric Constant

Temperature 25° C. (77° F.)

4.0-4.9

7.6-8.2

Temperature 60° C. (140° F.)

8.0-9.0

8.0-9.2

High Frequency—106 cycles—

After 48 hours at room temperature (75° F.)

60% R.H.

2.65-2.65

6.6-6.6

After 96 hours in water at 75° F.

6.24-7.55

10.8-11.6

Arc Resistance (ASTM D-495-38T)-

120-180 seconds

Chemical Properties —

- 1. Insoluble in water, but slightly absorbs water and water solutions.
- 2. Attacked by strong acids and alkalis.
- 3. Unaffected by alcohol, acetone, hydrocarbon solvents, oils and greases.
- 4. Odorless and tasteless.

(Except where noted tests were conducted by the American Cyanamid Company Laboratories, Stamford, Conn.)



APPLICATIONS OF MOLDED BEETLE

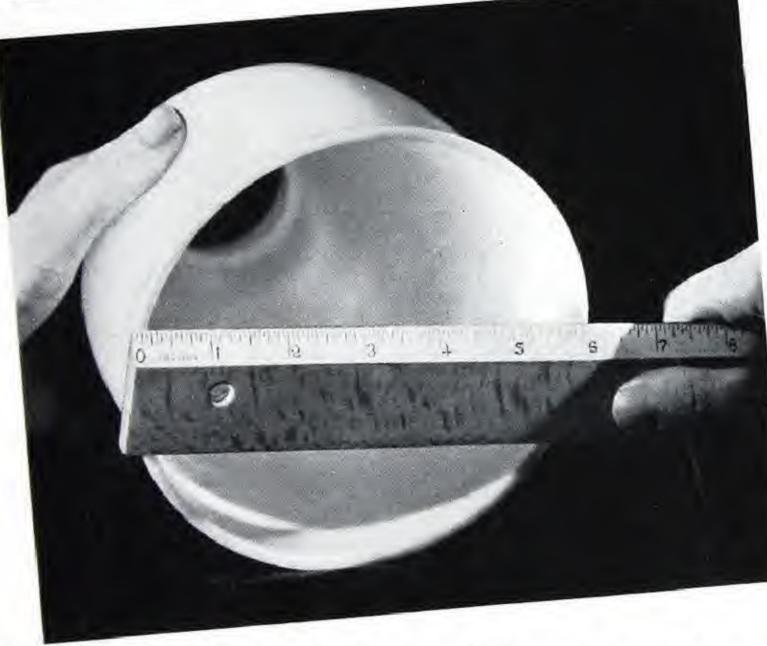
The enumeration below of applications for Beetle covers outstanding uses and will not attempt to mention all possibilities for the compound. New applications are occurring daily and may join those herein mentioned.

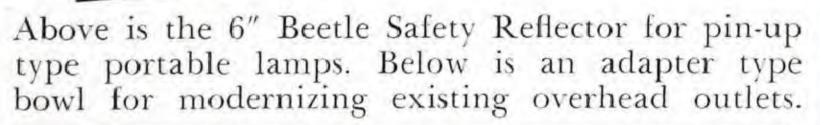
- 1. Buttons—Molded Beetle is used for buttons, decorative slides, clasps and buckles. The outstanding use in this field is for buttons on shirts, underwear, and pajamas.
- 2. Closures—Because of its brilliant colors and inertness Beetle is widely used for bottle caps and jar closures.
- 3. Housings—Beetle is used for radio cabinets, electric razor housings, clock cases, timer housings and a multitude of other smaller applications where color and permanence of finish are essential.
- 4. Tableware—Because of its light weight and strength Beetle is used in the form of tableware for yachts, trailers, airplanes, and picnic sets.
- 5. Containers—Molded Beetle is used for jewelry packages, cosmetic containers, cake boxes, cigarette and razor containers and a great variety of such applications where color stability, inertness, strength and resistance to wear are of importance.
- 6. Stove Handles—Colorful handles of Beetle decorate most kitchen stoves. Permanence of finish, color, and lack of heat conductivity are of importance.
- 7. Wiring Devices—Beetle is an excellent electrical insulator. It provides insulation, and color to blend with interior decorations.
- 8. Lighting—Beetle is used for lighting reflectors on portable lamps, for ceiling reflectors, automobile dome lenses, illuminated signs and displays. Beetle is eminently suitable for such applications for the following reasons:
 - A. It is available in practically any translucent color.
 - (1) The color and degree of light transmitted and reflected can be controlled and can be attuned to meet many different conditions.
 - B. Beetle reflectors are extremely lightweight and durable.
 - (1) A reflector molded of Beetle weighs about 1/3 as much as a similar reflector made of glass.
 - (2) It is strong and shatter-resistant. Reflectors as big as 24" in diameter are now being produced in Beetle.
 - C. It provides efficient lighting and illumination which is easy on the eyes. Reflectors with an efficiency of 87% are produced from Beetle material, and have a surface brightness of less than 2-candle power per square inch.
 - D. The light transmitted through Beetle is very diffused.
 - E. It is a safe and economical material for reflectors. Because of its light weight and strength, shipping costs and packaging costs are reduced. Cleaning and maintenance charges will be lower.





Left and above are two Beetle Safety Reflectors — the 8" and 9%" sizes — approved for use with I.E.S. lamps. Below is a large molded Beetle bowl for commercial installation.









We believe that the design and construction of Beetle lighting units require a study of special properties of the material, such as heat resistance, light transmission and reflection, color, life expectancy, etc. Our technical representatives will be glad to assist in the analysis of these problems.

DESIGN OF MOLDED BEETLE PARTS

We strongly advise that the buyer of molded parts, or the molder, construct a model of any new part before starting the die. This model should be analyzed in the light of good molding practice, service conditions after molding, and the physical and chemical properties of the plastic. The raw material supplier is always ready to lend assistance in this analysis.

Beetle in the mold becomes plastic by virtue of applied heat and pressure. As it flows throughout the mold, it is slowly stiffening and will eventually set. Perhaps the simplest part to mold is a shallow bowl of uniform wall thickness. Here there are no impediments to flow and if the die is correctly charged, the material will flow to the flash ports, set, and be ejected as a good part.

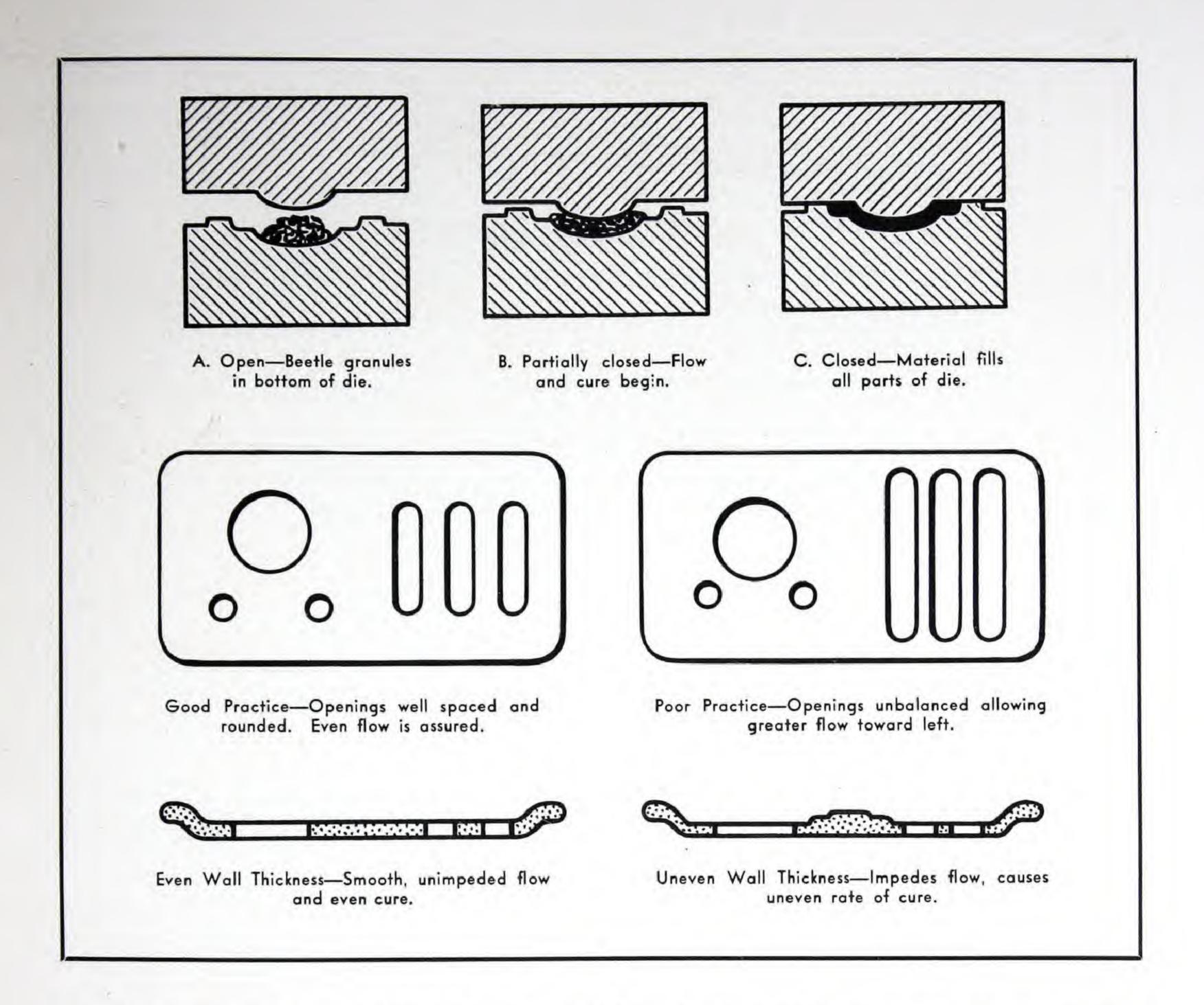
Since the basic molding process involves the shaping of a part by pressure applied in one axial direction, and the ejection of the piece along this same axis, the principles of metal casting design should be closely followed in the design of dies.

The most important fact to remember in designing molded parts is that walls or cross sections must be kept uniform in thickness. Non-uniform wall thickness leads to differentials in shrinkage, in flow and cure. The strains set up by such differentials will cause cracking and warping.

Side walls of pieces which form nearly a right angle with the base should be given a slight flare of one to two degrees for easy removal of the plunger and the molded part from the die. Right angles should be avoided. Such angles trap material or impede the material's flow. All corners or angles should have a small radius or fillet to permit the material to flow evenly throughout the piece.

Excessively thick walled sections should be avoided. Such sections are expensive and difficult to cure thoroughly. Core out the piece if possible.

If a flat section is to be molded having slots or openings in it, formed by baffles in the die, care must be taken to see that the material can flow at the same rate into all parts of the die and arrive in all localities at a uniform plasticity. If material is squirted through narrow slots because of uneven mold loading or non-uniform location of slots or baffles, it may not knit or bond properly.

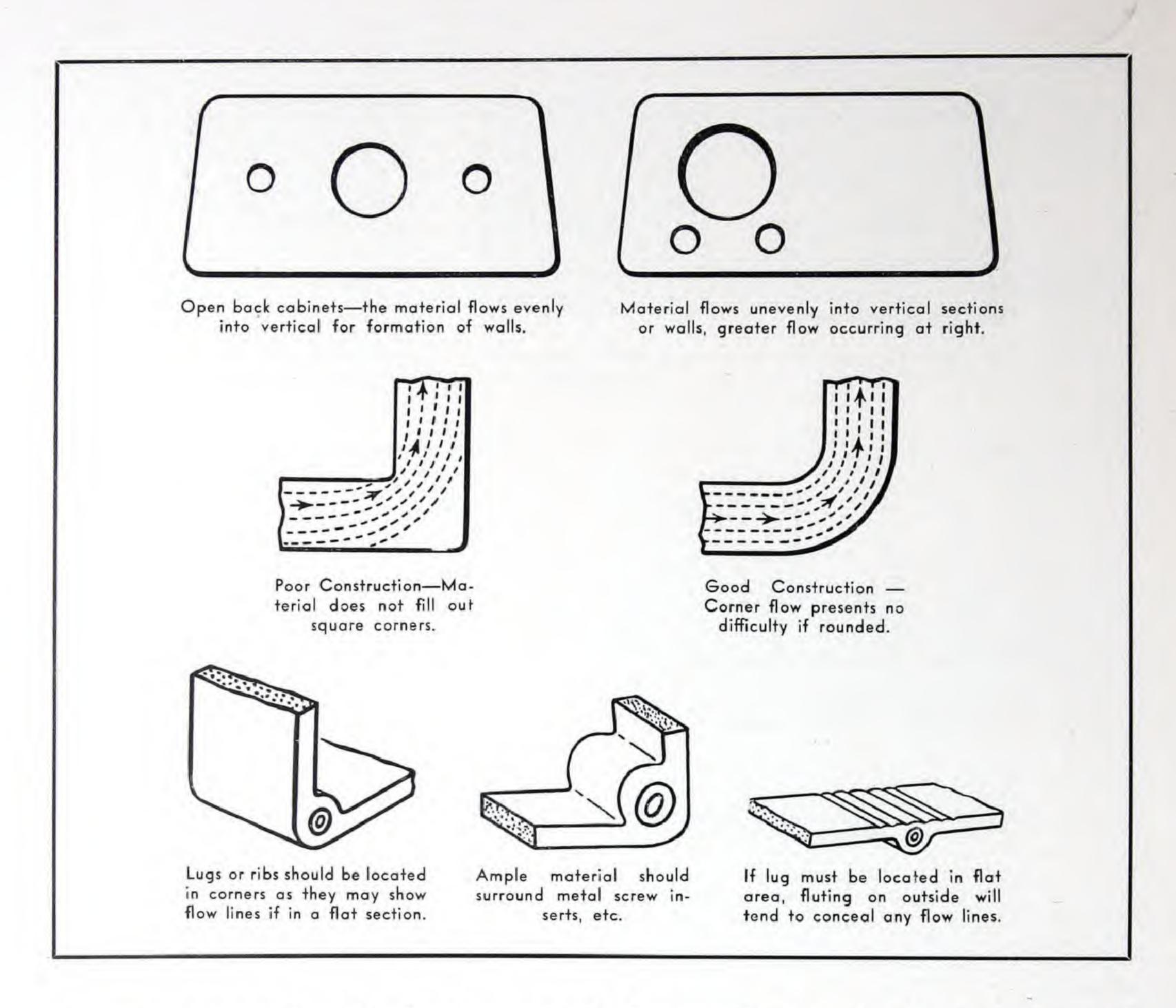


When material flows from the horizontal to the vertical, to form side walls, it must be permitted to flow uniformly. The angle at which the material leaves the horizontal and enters the vertical should be given an ample radius. Pressure should be constantly on the material, and the design should be such that the compound flows to the top of the die in a uniformly plastic condition. Heavy sections at the top of the die should be avoided.

If baffles occur in the side wall to form dial openings, slots, or holes, they should be rounded, uniformly spaced, and placed as near the bottom of the die as possible. Such baffles should be quite far from each other to permit the passage of material around them. The ribs of radio grills should be as short as possible and uniform in thickness.

Drilling of large holes in the lighter sections of molded pieces is not advised. Drilling may start small cracks which will spread as the material ages.

If a radio cabinet is being designed it would be well to locate the tubes of the set as

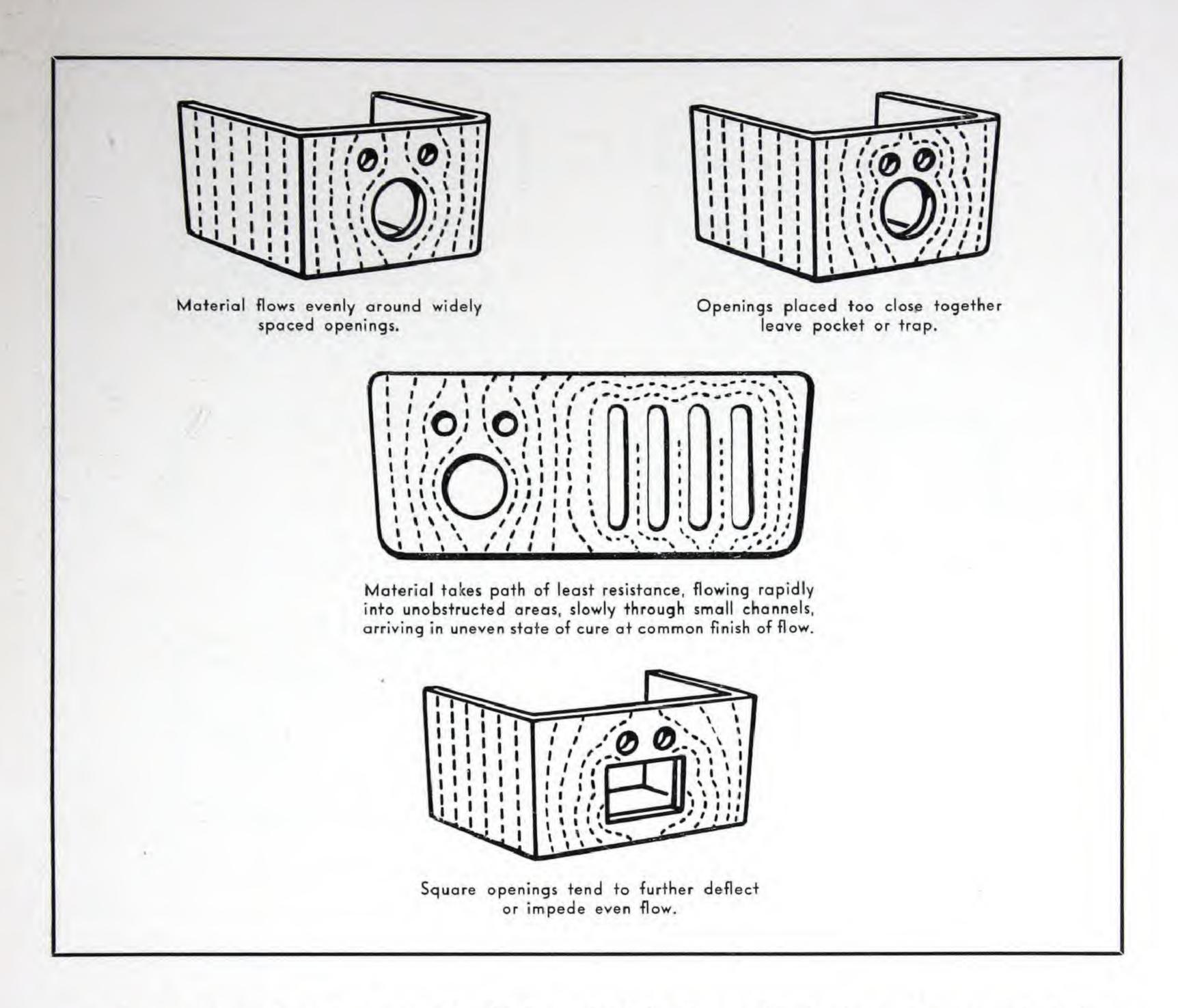


far away as possible from the Beetle surface. If they must be near the plastic, the material should be ventilated or painted with a heat reflecting paint.

Bosses should be located in the corners of molded pieces. Here there is an abundance of material during the molding operation, and flow lines or shadows which may occur from a thick cross section in a translucent material will be avoided. If bosses are located in the side walls, some decorative fluting may be placed on the outer face to conceal the shadow or flow lines.

Always locate flash lines where they will not be seen, preferably along a decorative line or edge.

Molded parts should be permitted to alter their dimensions in varying atmospheric conditions. If ureas are held rigidly in place, or are bolted to another material which has a different rate of dimensional change, they may crack.



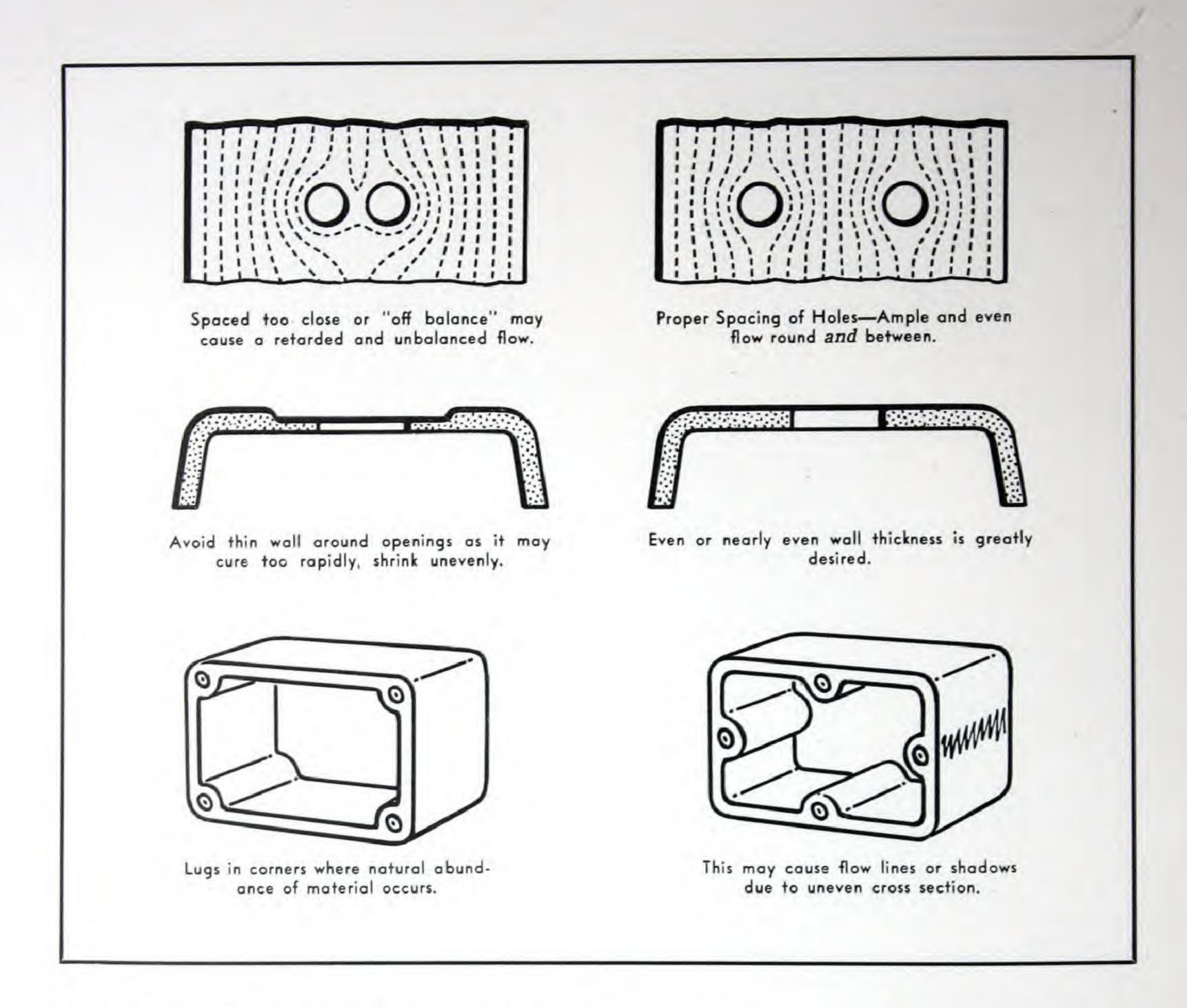
Decorations, lettering, etc. should be raised in the molded piece. Depressed designs mean raised designs cut on the steel; this work is expensive.

Molded holes should have a ratio of length to diameter of not more than 2½ to 1 if possible. This will prevent binding or breakage of mold pins.

Metal inserts may be used but care must be taken to see that they are strong and thoroughly anchored in the die. The insert should occur where there is an abundance of material in the parts. Thin plastic walls around an insert will crack.

Inserts should be heavily knurled and should protrude beyond the molded surface. If the insert is flush with the piece, material may flow into it or around it, causing an expensive cleaning operation.

Hexagonal inserts are apt to cause trouble and expense. A hexagonal hole is expen-



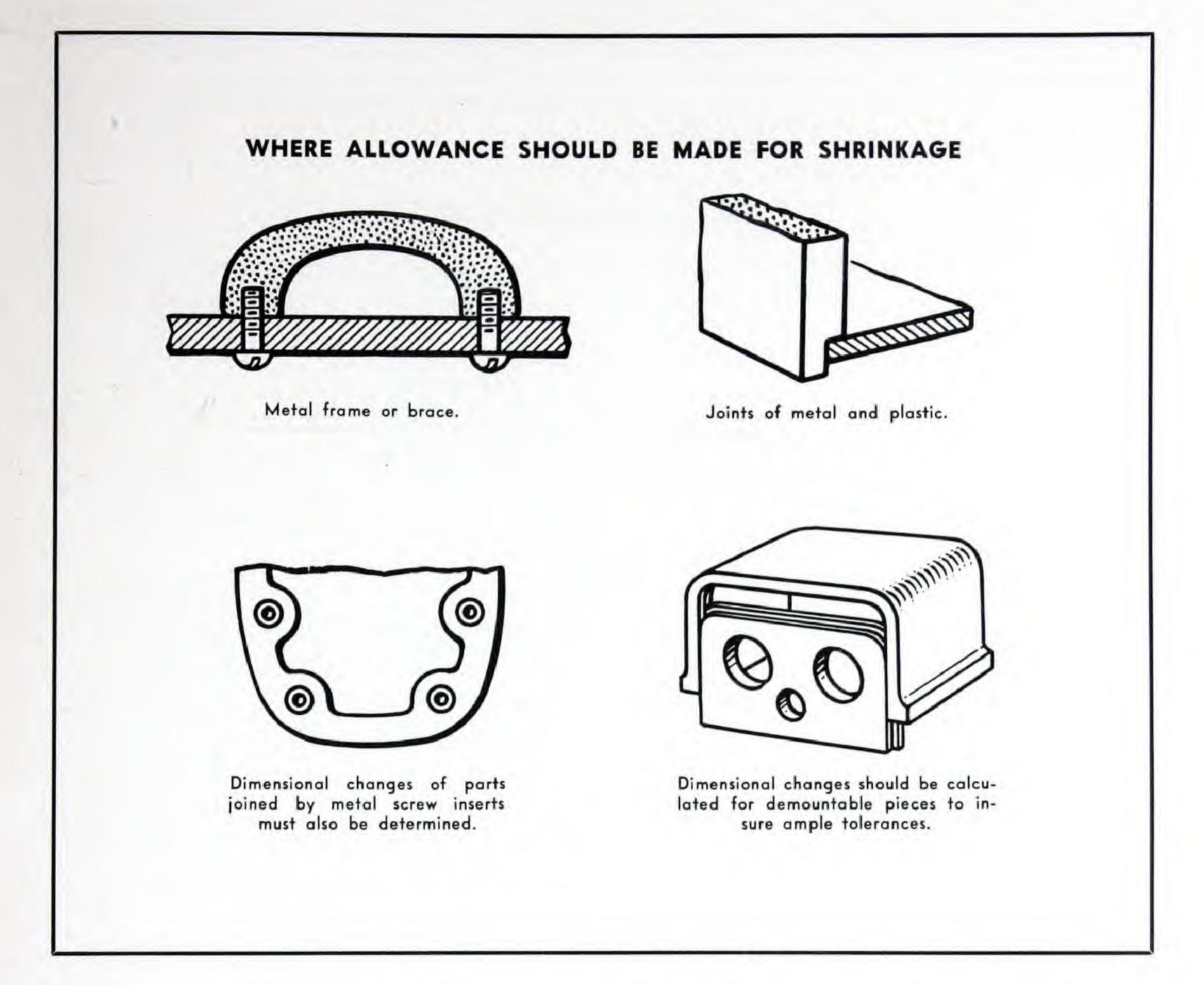
sive to cut in the die, and the hexagonal insert presents sharp corners which may cause the plastic to crack.

Don't call for blind holes or inserts in the side wall of a piece where the depth of the hole or the length of the insert is greater than twice its breadth.

Frequently the trouble and expense of placing inserts in a molded piece can be avoided through the use of drive screws. Holes may be molded into the piece at no extra cost, and the assembly is made by using these screws without slowing up the operations at the press. These screws do not lend themselves to disassembly.

TAPPING AND DRILLING OF MOLDED BEETLE

Specific instructions cannot be given as the method of operation varies with the size and depth of hole and whether the hole is to be drilled through or is blind. Drill speeds are



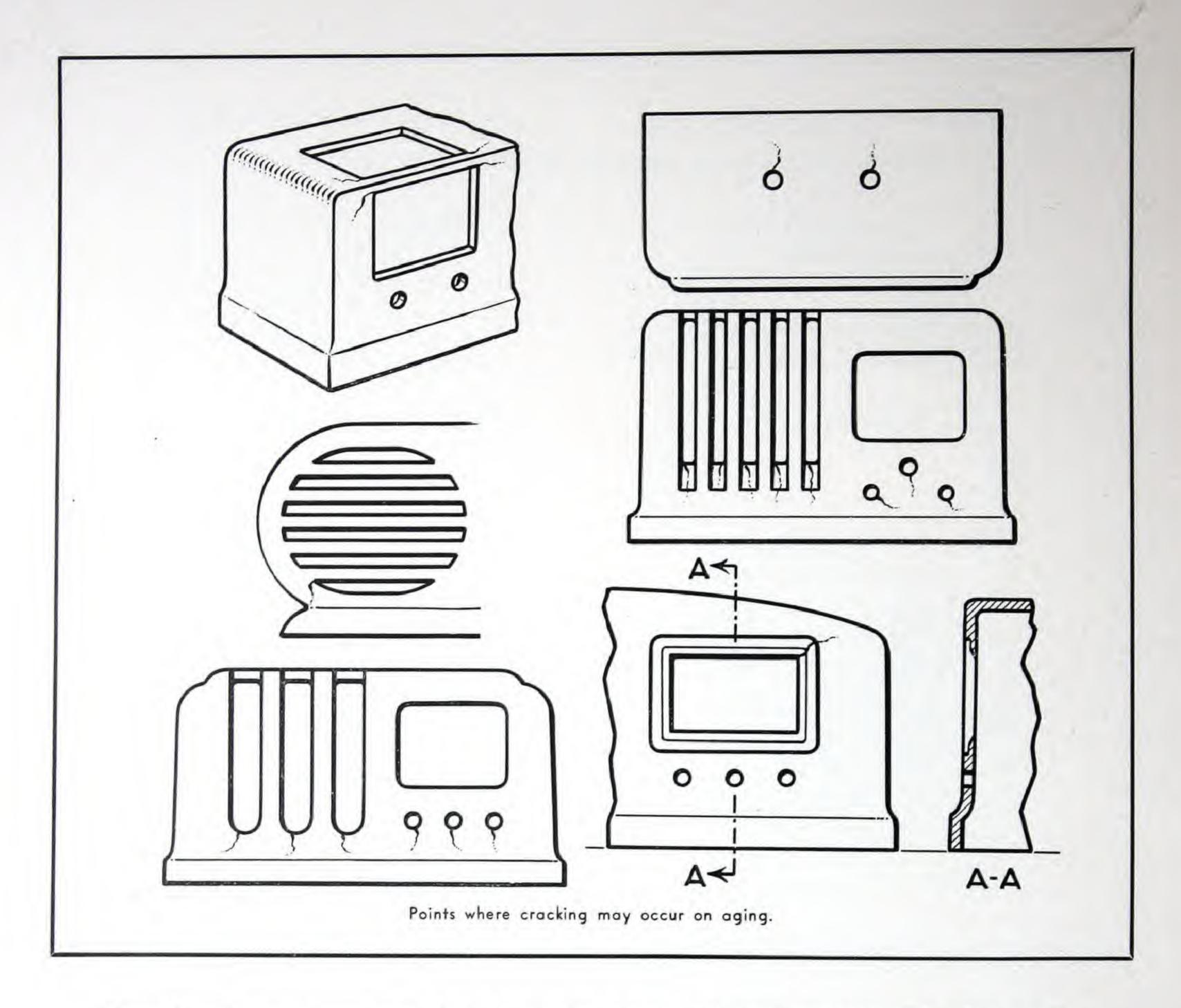
comparable to those used in drilling metal. Small drills are run at high speeds; large drills at low speeds.

Blind holes are drilled with a standard cutting angle, whereas through holes are usually made with a drill having a more tapered cutting edge in order to reduce chipping as the drill comes through the piece.

Variations in the density or hardness of the part are compensated for by altering the included angle of the cutting point of the drill. Hard materials are drilled using the standard angle of about 118°, and soft materials are best drilled using a more acute angle $(90^{\circ}-60^{\circ})$ on the drill.

If drilled holes are to be tapped, a drill two or three numbers larger than the size used in drilling steel should be used. A blind drilled hole should be tapped only 75% of its depth. And taps for this purpose should have the lead removed before they are used.

For drilling through holes in thin sections, slow helix or even straight fluted drills are advantageous.



Tapping is not recommended for holes above ½" in diameter. The larger the tap the sooner it dulls and the more the thread will chip. Above this size use a brass insert. If the piece is to be reassembled many times, the molded insert is preferable.

Do not call for unnecessarily close tolerances.

In all cases place full confidence in your molder and treat him as a consulting engineer in whom you can confide. Let him know how your part will be used, what its life expectancy is to be, and the volume of items you will require. If the application for your part is new follow this procedure:

- 1. Obtain samples of the plastic you want to use, and test them under service conditions as closely approximating your conditions as possible.
- 2. Construct a model of the part with the advice of your molder or raw material supplier.
 - 3. When model is acceptable, build a single cavity die to produce the actual part.
 - 4. If this serves the purpose contemplated, construct the regular production die.

MATERIALS COMPARISON TABLE

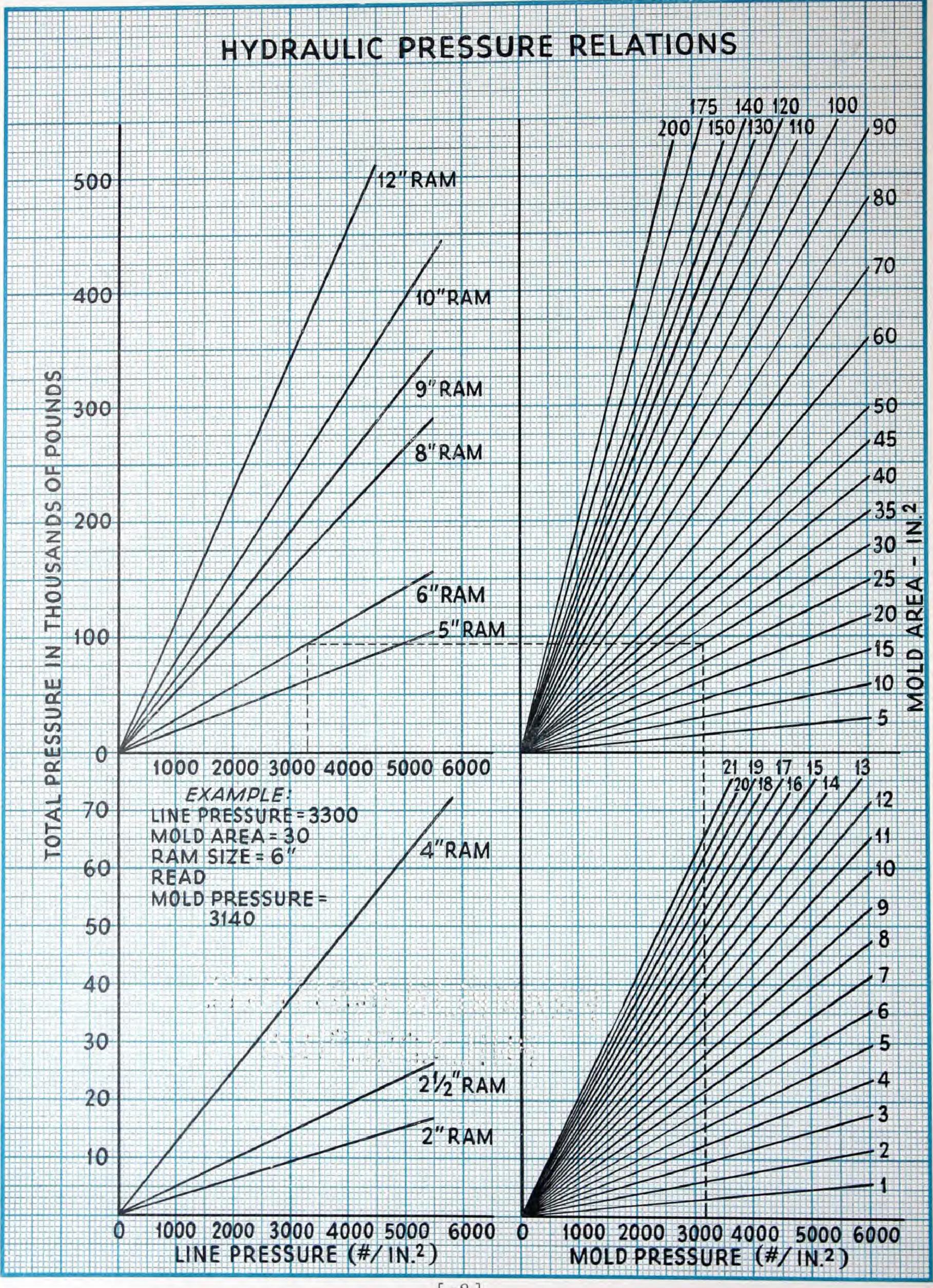
MATERIAL	SPECIFIC GRAVITY	WEIGHT (Per Cu. In.)	(Lbs. per Sq. Inch)
Beetle	1.45-1.50	0.85-0.89 oz.	5500-7000

METALS

2.67	1.538 oz.	30000-40000
8.40	4.838 oz.	45000-85000
8.853	5.099 oz.	60000-70000
7.854	4.524 oz.	80000-330000
7.35	4.234 oz.	4000-5000
7.0	4.032 oz. (cast)	7000-13000
	8.40 8.853 7.854 7.35	8.40 4.838 oz. 8.853 5.099 oz. 7.854 4.524 oz. 7.35 4.234 oz.

MISCELLANEOUS MATERIALS

Glass	2.6-3.7	1.498-2.131 oz.	Up to 13,000
Mica	2.9	1.670 oz.	15,000 shear lb. per sq. in
Porcelain	2.4	1.382 oz.	3,000
Rubber, Hard (Commercial Grade) Wood	J.15-1.4	C.6424-0.8064 oz.	4000-8000
(Hard Maple)	0.68 (average)	. 03917 oz., (average)	26,000
(Soft-W. Pine)	0.45 (average)	0:2592 oz. (average)	17,300



				CA	PA	C	TII	ES	0	F	HY	DR	AU	LIC	C	RA	MS	11	Ν.	ТО	NS				
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-																					7000 2.76	Inch	Ft.		
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2 1/2	0.47	0.79	0.94	1.18	1.57	1.88	2.36	2.83	3.14	3.53	3.93	4.32	4.71	5.50	6.28	7.07	7.85	8.64	9.42	10.2	11.0	.014	.163	3.14	2
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4	1.88	3.14	3.77	4.71	6.28	7.54	9.42	11.3	12.6	14.1	15.7	17.3	18.8	22,0	25,1	28.3	31.4	34.6	37.7	40.8	44.0	.054	.653	12.6	4
5	2.95	4.91	5.89	7.36	9.82	11.8	14.7	17.7	15.9	17.9	19.9	21.9	23.9	27.8 34.3	31.8	35.8	39.8	43.7	47.7 58.9	51.7 63.8	55.7 68.7	.069	1.02	15.9 19.6	41/2
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6	4.24	7.07	8.48	10.6	14.1	17.0	21.2	25.4	28.3	31.8	35.3	38.9	42.4	49.5	56.5	63.6	70.7	77.8	84.8	91.9	99.0	.122	1.47	28.3	51/2
61/2	4.98 5.77	9.62	9.96	12.4	16.6	19.9	24.9	29.9	33.2	37.3	41.5	45.6	49.8	58.1	66.4	74.7	83.0 96.2	91.3	99.6	108	116	14.5.00			
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48	271 283	452 471	543 566	679 707	905	1086	1357	1629	1810	2036	2262	2488	2714	3167	3619	4072	4524	4976	5429	5881	6333	7.83	94.0	1810	48
50	295	491	589	736	943		1473										4714 4909					5		1886 1963	
52	319	531	637	796	1060	1270	1590						100			1500		600			7430				
54	344	573	687	859	1150	1370	1720	2060	2290	2580	2860	3150	3440	4010	4580	5150	5730	6300	6870	7440	8020	9.91	119	2124 2290	100
56 58	369	616	739	924	1320	1480	1850	2220	2460	2770	3080	3390	3690	4310	4930	5540	6160	6770	7390	8000	8620 9250	10.7	128	2463	56
60	424	707	848	1060	1410	1700	2120	2540	2830	3180	3530	3890	4240	4950	5650	6360	7070	7780	8480	9190	9900	12.2	147	2827	60
	.175	. 292	. 350	. 438	. 583	.700	. 875	1.05	1.17	1.31	1.46	1.60	1.75	2.04	2.33	2.62	2.92	3.21	3.50	3.79	4.08	Н. Р	. per	gal, pe	r min.

CONVERSION OF VOLUMES OR CUBIC MEASURE

	Cubic Inches to Cubic Centimeters	Cubic Centimeters to Cubic Inches	Cubic Feet to Cubic Meters	Cubic Meters to Cubic Feet	Cubic Yards to Cubic Meters	Cubic Meters to Cubic Yards	Gallons to Cubic Feet	Cubic Feet to Gallons
1	16.39	0.06102	0.02832	35.31	0.7646	1.308	0.1337	7.481
2	32.77	0.1220	0.05663	70.63	1.529	2.616	0.2674	14.96
3	49.16	0.1831	0.08495	105.9	2.294	3.924	0.4011	22.44
4	65.55	0.2441	0.1133	141.3	3.058	5.232	0.5348	29.92
5	81.94	0.3051	0.1416	176.6	3.823	6.540	0.6685	37.41
6	98.32	0.3661	0.1699	211.9	4.587	7.848	0.8022	44.89
7	114.7	0.4272	0.1982	247.2	5.352	9.156	0.9359	52.36
8	131.1	0.4882	0.2265	282.5	6.116	10.46	1.070	59.85
9	147.5	0.5492	0.2549	317.8	6.881	11.77	1.203	67.33

DECIMAL EQUIVALENTS OF FRACTIONS OF ONE INCH

1/64	.015	625	17/64	.265	625	33/64	.515	625	49/64	.765	625
1/32	.031	250	9/32	.281	250	17/32		250	25/32		250
3/64	.046	875	19/64	.296	875	35/64	.546		51/64		875
1/16	.062	500	5/16	.312	500	9/16		500	13/16	.812	
5/64	.078	125	21/64	.328	125	37/64	.578	125	53/64	.828	125
3/32	.093	750	11/32	.343	750	19/32	.593	750	27/32		750
7/64	.109	375	23/64	.359	375	39/64	.609		55/64	.859	
1/8	.125	000	3/8	.375	000	5/8	.625		7/8	.875	
9/64	.140	625	25/64	.390	625	41/64	.640	625	57/64	.890	625
5/32	.156	250	13/32	.406	250	21/32	.656		29/32	.906	
11/64	.171	875	27/64	.421	875	43/64	.671	200	59/64	.921	
3/16	.187	500	7/16	.437	500	11/16	.687		15/16	.937	
13/64	.203	125	29/64	.453	125	45/64	.703	125	61/64	.953	125
7/32	.218	750	15/32	.468	750	23/32	.718	and the second s	31/32	.968	
5/64	.234	375	31/64	.484	375	47/64	.734		63/64	.984	
1/4	.250	000	1/2	.500		3/4	.750		33/01	1.000	

TAP AND DRILL SIZES

Size of Tap, No.	Size of Drill, No.	Size of Tap, No.	Size of Drill, No.	Size of Tap, No.	Size of Drill, No.	Size of Tap, No.	Size of Drill No.
2 x 48	50	7 x 32	30	13 x 20	15	18 x 20	A
2 x 56	49	8 x 24	30	13 x 22	15	19 x 16	A
2 x 64	48	8 x 30	30	13 x 24	13	19 x 18	č
3 x 40	47	8 x 32	29	14 x 20	13	19 x 20	Ď
3 x 48	45	9 x 24	29	14 x 22	İÌ	20 x 16	Ď
3 x 56	44	9 x 28	28	14 x 24	9	20 x 18	F
4 x 32	43 42	9 x 30	27	15 x 18		20 x 20	Ĥ
4 x 36		9 x 32	25	15 x 20	10	22 x 16	3
4 x 40	41	10 x 24	25	15 x 22		22 x 18	ĭ
5 x 30	40	10 x 30	22	15 x 24	6	24 x 14	й
5 x 32	40	10 x 32	21	16 x 16	7	24 x 16	N
5 x 36	38 37	11 x 24	21	16 x 18	6	24 x 18	Ö
5 x 40	37	11 x 28	17	16 x 20	5	26 x 14	ŏ
6 x 30	35	11 x 30	17	17 x 16		26 x 16	P
6 x 32	35	12 x 20	19	17 x 18	2	28 x 14	P
6 x 36	33	12 x 22	17	17 x 20	2 2	28 x 16	Š
6 x 40	32	12 x 24	17	18 x 16	2	30 x 14	ŭ
7 x 28	32 31	12 x 28	15	18 x 18	1	30 x 16	v
7 x 30	31						36

TEMPERATURE CONVERSION TABLES

NOTE:—The numbers in bold face type refer to the temperature either in degrees Centigrade or Fahrenheit which it is desired to convert into the other scale. If converting from Fahrenheit degrees to Centigrade degrees the equivalent temperature will be found in the left column, while if converting from degrees Centigrade to degrees Fahrenheit, use the column on the right.

C.		F.	C.		F.	C.		F.	C.		F.	C.		F.
-17.8	0	32	15.0	59	138.2	132	270	518	454	850	1562	777	1430	2606
-17.2	1	33.8	15.6	60	140.0	138	280	536	460	860	1580	782	1440	2624
-16.7	2	35.6	16.1	61	141.8	143	290	554	466	870	1598	788	1450	2642
-16.1	3	37.4	16.7	62	143.6	149	300	572	471	880	1616	793	1460	2660
-15.6	4	39.2	17.2	63	145.4	154	310	590	477	890	1634	799	1470	2678
-15.0	5	41.0	17.8	64	147.2	160	320	608	482	900	1652	804	1480	2696
-14.4	6	42.8	18.3	65	149.0	166	330	626	488	910	1670	810	1490	2714
-13.9	7	44.6	18.9	66	150.8	171	340	644	493	920	1688	816	1500	2732
-13.3	8	46.4	19.4	67	152.6	177	350	662	499	930	1706	821	1510	2750
-12.8	9	48.2	20.0	68	154.4	182	360	680	504	940	1724	827	1520	2768
-12.2	10	50.0	20.6	69	156.2	188	370	698	510	950	1742	832	1530	2786
-11.7	11	51.8	21.1	70	158.0	193	380	716	516	960	1760	838	1540	2804
-11.1	12	53.6	21.7	71	159.8	199	390	734	521	970	1778	843	1550	2822
-10.6	13	55.4	22.2	72	161.6	204	400	752	527	980	1796	849	1560	2840
-10.0	14	57.2	22.8	73	163.4	210	410	770	532	990	1814	854	1570	2858
- 9.44	15	59.0	23.3	74	165.2	216	420	788	538	1000	1832	860	1580	2876
- 8.89	16	60.8	23.9	75	167.0	221	430	806	543	1010	1850	866	1590	2894
- 8.33	17	62.6	24.4	76	168.8	227	440	824	549	1020	1868	871	1600	2912
— 7.78	18	64.4	25.0	77	170.6	232	450	842	554	1030	1886	877	1610	2930
- 7.22	19	66.2	25.6	78	172.4	238	460	860	560	1040	1904	882	1620	2948
- 6.67	20	68.0	26.1	79	174.2	243	470	878	566	1050	1922	888	1630	2966
- 6.11	21	69.8	26.7	80	176.0	249	480	896	571	1060	1940	893	1640	2984
- 5.56	22	71.6	27.2	81	177.8	254	490	914	577	1070	1958	899	1650	3002
- 5.00	23	73.4	27.8	82	179.6	260	500	932	582	1080	1976	904	1660	3020
- 4.44	24	75.2	28.3	83	181.4	266	510	950	588	1090	1994	910	1670	3038
- 3.89	25	77.0	28.9	84	183.2	271	520	968	593	1100	2012	916	1680	3056
- 3.33	26	78.8	29.4	85	185.0	277	530	986	599	1110	2030	921	1690	3074
- 2.78	27	80.6	30.0	86	186.8	282	540	1004	604	1120	2048	927	1700	3092
_ 2.22	28	82.4	30.6	87	188.6	288	550	1022	610	1130	2066	932	1710	3110
- 1.67	29	84.2	31.1	88	190.4	293	560	1040	616	1140	2084	938	1720	3128
- 1.11	30	86.0	31.7	89	192.2	299	570	1058	621	1150	2102	943	1730	3146
0.54	31	87.8	32.2	90	194.0	304	580	1076	627	1160	2120	949	1740	3164
0.50	32	89.6	32.8	91	195.8	310	590	1094	632	1170	2138	954	1750	3182
0.56	33	91.4	33.3	92	197.6	316	600	1112	638	1180	2156	960	1760	3200
1.11	34	93.2	33.9	93	199.4	321	610	1130	643	1190	2174	966	1770	3218
1.67	35	95.0	34.4	94	201.2	327	620	1148	649	1200	2192	971	1780	3236
2.22	36	96.8	35.0	95	203.0	332	630	1166	654	1210	2210	977	1790	3254
2.78	37	98.6	35.6	96	204.8	338	640	1184	660	1220	2228	982	1800	3272
3.33	38	100.4	36.1	97	206.6	343	650	1202	666	1230	2246	988	1810	3290
3.89	39	102.2	36.7	98	208.4	349	660	1220	671	1240	2264	993	1820	3308
4.44	40	104.0	37.2	99	210.2	354	670	1238	677	1250	2282	999	1830	3326
5.00	41	105.8	37.8	100	212.0	360	680	1256	682	1260	2300	1004	1840	3344
5.56	42	107.6	43	110	230	366	690	1274	688	1270	2318	1010	1850	3362
	43	109.4	49	120	248	371	700	1292	693	1280	2336	1016	1860	3380
6.11	44	111.2	54	130	266	377	710	1310	699	1290	2354	1021	1870	3398
7.67% 4/3/9	45	113.0	60	140	284	382	720	1328	704	1300	2372	1027	1880	3416
7.22	46	114.8	66	150	302	388	730	1346	710	1310	2390	1032	1890	3434
7.78	47	116.6	71	160	320	393	740	1364	716	1320	2408	1038	1900	3452
8.33	48	118.4	77	170	338	399	750	1382	721	1330	2426	1043	1910	3470
8.89			82	180	356	404	760	1400	727	1340	2444	1049	1920	3488
9.44	49 50	120.2	88	190	374	410	770	1418	732	1350	2462	1054	1930	3506
10.0			93	200	392	416	780	1436	738	1360	2480	1060	1940	3524
10.6	51	123.8	99	210	410	421	790	1454	743	1370	2498	1066	1950	3542
11.1	52	125.6	1000	212	413	427	800	1472	749	1380	2516	1071	1960	3560
11.7	53	127.4	100	220	428	432	810	1490	754	1390	2534	1077	1970	3578
12.2	54	129.2	104		446	438	820	1508	760	1400	2552	1082	1980	3596
12.8	55	131.0	110	230	464	443	830	1526	766	1410	2570	1088	1990	3614
13.3	56	132.8	116	240		449	840	1544	771	1420	2588	1093	2000	3632
13.9	57	134.6	121	250	482	777	040	1544	111	1420	2500	1073	2000	3032
14.4	58	136.4	127	260	500									

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